PRODUCT FEATURES

- High and critical load applications.
- Excellent for chemical resistance fixings.
- Fire resistance up to 240 minutes in concrete structure.
- For use in dry and wet concrete.
- · High durability; tested based on a 50 years working life of anchor according to ETA.
- Structural applications in cracked and uncracked concrete applications in seismic

RESIN SPECIFICATIONS

- 100% Solid Epoxy Resin grey after mixing.
- Specific weight: 1.5 g/cm³.
- Compressive strength (ASTM D 695): 95 N/mm².

• Shelf life is 24 months with the cartridges stored in their original packing, the correct way up and in cool dry conditions (+5°C to +25°C) out of direct sunlight.

SUBSTRATES

- RC concrete C20/25 to C50/60 at maximum according to EN 206-1:2000-12.
- Solid stone & other solid masonry.



HOLE ORIENTATION





LOADING ZONES





APPROVALS / CERTIFICATIONS

- ETA-17/0410 according to ETAG 001 Part 1 & 5 Option 1.
- CE Certified No. 1020-CPR-090-038603.
- Seismic Performance Report.
- F240 Fire Test Report No. 26069571/B.
- LEED 2009 EQ c4.1 SCAQMD rule 1168 (2005).
- VOC A+ Rating (Volatile Organic Compound).
- WRAS No. 1510550 according to BS6920-1:2014.
- Creep Test Certificate No. 15/10972-1820-S.













VA RODS AVAILABILITY









BASIC LOADING DATA

- For static and quasi-static loadings.
- Only a single anchor is considered.
- No anchor spacing and edge distance influences.
- Loading applicable to dry and wet concrete.
- Concrete compressive strength C20/25 (f_{ck,cube} = 25 N/mm²).
 Loading based on standard anchorage depth.
- For non-cracked and cracked concrete.
- Loading data conformed to ETA-17/0410, except M8 and M27.

| CHARACTERISTIC RESISTANCE [F _{Rk}] | | | | | | | | STEEL | CLASS 5.8 |
|--|------|------|------|------|------------|------------|-------|-------|-----------|
| Anchor Size | | M8 | M10 | M12 | M16 | M20 | M24 | M27 | M30 |
| | | | | ı | Non-Cracke | ed Concret | e | | |
| Tensile Load, N _{Rk} | [kN] | 18.0 | 29.0 | 42.0 | 69.1 | 111.9 | 153.7 | 199.6 | 224.0 |
| Shear Load, V _{Rk} | [kN] | 9.0 | 15.0 | 21.0 | 39.0 | 61.0 | 88.0 | 115.0 | 140.0 |
| | | | | | Cracked | Concrete | | | |
| Tensile Load, N _{Rk} | [kN] | 17.1 | 24.0 | 35.3 | 50.3 | 58.8 | 87.1 | 116.6 | 140.0 |
| Shear Load, V _{Rk} | [kN] | 9.0 | 15.0 | 21.0 | 39.0 | 61.0 | 88.0 | 115.0 | 140.0 |

| DESIGN RESISTANCE [F _{Rd}] | | | | | | | | | |
|--------------------------------------|------|------|------|------|---------|----------|------|-------|-------|
| Anchor Size | | M8 | M10 | M12 | M16 | M20 | M24 | M27 | M30 |
| Non-Cracked Concrete | | | | | | | | | |
| Tensile Load, N _{Rd} | [kN] | 12.0 | 17.3 | 21.7 | 32.9 | 56.0 | 90.5 | 101.0 | 121.2 |
| Shear Load, V _{Rd} | [kN] | 7.2 | 12.0 | 16.8 | 31.2 | 48.8 | 70.4 | 92.0 | 112.0 |
| | | | | | Cracked | Concrete | | | |
| Tensile Load, N _{Rd} | [kN] | 9.5 | 13.4 | 16.8 | 25.4 | 28.0 | 41.5 | 55.5 | 66.7 |
| Shear Load, V _{Pd} | [kN] | 7.2 | 12.0 | 16.8 | 31.2 | 48.8 | 70.4 | 92.0 | 112.0 |

| RECOMMENDED LOAD [F _{Rec}] | | | | | | | | | |
|--------------------------------------|------|-----|------|------|------------|-------------|------|------|------|
| Anchor Size | | M8 | M10 | M12 | M16 | M20 | M24 | M27 | M30 |
| | | | | I | Von-Cracke | ed Concrete | е | | |
| Tensile Load, N _{Rec} | [kN] | 8.6 | 12.3 | 15.5 | 23.5 | 40.0 | 64.6 | 72.1 | 86.6 |
| Shear Load, V _{Rec} | [kN] | 5.1 | 8.6 | 12.0 | 22.3 | 34.9 | 50.3 | 65.7 | 80.0 |
| | | | | | Cracked | Concrete | | | |
| Tensile Load, N _{Rec} | [kN] | 6.8 | 9.5 | 12.0 | 18.2 | 20.0 | 29.6 | 39.7 | 47.6 |
| Shear Load, V _{Rec} | [kN] | 5.1 | 8.6 | 12.0 | 22.3 | 34.9 | 50.3 | 65.7 | 80.0 |

^{*} Bold Italic numbers represent steel failure.



| COO MIGHT ERI ORWA | _ | | OXI | | VAIN | | | oncrete Capa | |
|--|------|------|------|------|-----------|------------|----------|--------------|----------|
| CHARACTERISTIC RESISTANCE [F _{Rk}] | | | | | | | HIGH TEN | ISILE STEEL | CLASS 8 |
| Anchor Size | | M8 | M10 | M12 | M16 | M20 | M24 | M27 | M30 |
| | | | 1 | | Non-Crack | ed Concret | e | 1 | |
| Tensile Load, N _{Rk} | [kN] | 22.1 | 31.1 | 45.6 | 69.1 | 111.9 | 153.7 | 199.6 | 224. |
| Shear Load, $V_{\rm Rk}$ | [kN] | 15.0 | 23.0 | 34.0 | 63.0 | 98.0 | 141.0 | 184.0 | 224. |
| | | | | | Cracked | Concrete | | | |
| Tensile Load, N _{Rk} | [kN] | 17.1 | 24.0 | 35.3 | 50.3 | 58.8 | 87.1 | 116.6 | 140. |
| Shear Load, V _{Rk} | [kN] | 15.0 | 23.0 | 34.0 | 63.0 | 98.0 | 141.0 | 184.0 | 224. |
| DESIGN RESISTANCE [F _{Rd}] | | | | | | | | | |
| Anchor Size | | M8 | M10 | M12 | M16 | M20 | M24 | M27 | M30 |
| | | | | | Non-Crack | ed Concret | e | | |
| Tensile Load, N _{Rd} | [kN] | 12.3 | 17.3 | 21.7 | 32.9 | 56.0 | 90.5 | 101.0 | 121. |
| Shear Load, $V_{_{Rd}}$ | [kN] | 12.0 | 18.4 | 27.2 | 50.4 | 78.4 | 112.8 | 147.2 | 179. |
| | | | | | Cracked | Concrete | | | |
| Tensile Load, N _{Rd} | [kN] | 9.5 | 13.4 | 16.8 | 25.4 | 28.0 | 41.5 | 55.5 | 66.7 |
| Shear Load, V _{Rd} | [kN] | 12.0 | 18.4 | 27.2 | 50.4 | 78.4 | 112.8 | 147.2 | 179. |
| RECOMMENDED LOAD [F _{sor}] | | | | | | | | | |
| Anchor Size | | M8 | M10 | M12 | M16 | M20 | M24 | M27 | M30 |
| | | | | | Non-Crack | ed Concret | e | | |
| Tensile Load, N _{Rec} | [kN] | 8.8 | 12.3 | 15.5 | 23.5 | 40.0 | 64.6 | 72.1 | 86.6 |
| Shear Load, V _{Rec} | [kN] | 8.6 | 13.1 | 19.4 | 36.0 | 56.0 | 80.6 | 105.1 | 128.0 |
| | | | | | Cracked | Concrete | | | |
| Tensile Load, N _{Rec} | [kN] | 6.8 | 9.5 | 12.0 | 18.2 | 20.0 | 29.6 | 39.7 | 47.6 |
| Shear Load, V _{Rec} | [kN] | 8.6 | 13.1 | 19.4 | 36.0 | 56.0 | 80.6 | 105.1 | 128.0 |
| Bold Italic numbers represent steel failure. | | | | | | | | | |
| | | | | | | | | | |
| CHARACTERISTIC RESISTANCE [F _{Rk}] | | | | | | | STAINLES | S STEEL CLA | SS A2/A4 |
| Anchor Size | | M8 | M10 | M12 | M16 | M20 | M24 | M27 | M30 |
| | | | | | Non-Crack | ed Concret | е | | |
| Tensile Load, N _{Rk} | [kN] | 22.1 | 31.1 | 45.6 | 69.1 | 111.9 | 153.7 | 199.6 | 224.0 |
| Shear Load, V _{Rk} | [kN] | 13.0 | 20.0 | 30.0 | 55.0 | 86.0 | 124.0 | 161.0 | 196.0 |

| CHARACTERISTIC RESISTANCE [F _{Rk}] | | | | | | | STAINLES | S STEEL CLA | SS A2/A4 |
|--|------|----------------------|------|------|------------|------------|----------|-------------|----------|
| Anchor Size | | М8 | M10 | M12 | M16 | M20 | M24 | M27 | M30 |
| | | | | ı | Non-Cracke | ed Concret | e | | |
| Tensile Load, N _{Rk} | [kN] | 22.1 | 31.1 | 45.6 | 69.1 | 111.9 | 153.7 | 199.6 | 224.0 |
| Shear Load, $V_{\rm Rk}$ | [kN] | 13.0 | 20.0 | 30.0 | 55.0 | 86.0 | 124.0 | 161.0 | 196.0 |
| | | | | | Cracked | Concrete | | | |
| Tensile Load, N _{Rk} | [kN] | 17.1 | 24.0 | 35.3 | 50.3 | 58.8 | 87.1 | 116.6 | 140.0 |
| Shear Load, V _{Rk} | [kN] | 13.0 | 20.0 | 30.0 | 55.0 | 86.0 | 124.0 | 161.0 | 196.0 |
| DESIGN RESISTANCE [F _{au}] | | | | | | | | | |
| Anchor Size | | M8 | M10 | M12 | M16 | M20 | M24 | M27 | M30 |
| | | Non-Cracked Concrete | | | | | | | |
| Tensile Load, N _{Rd} | [kN] | 12.3 | 17.3 | 21.7 | 32.9 | 56.0 | 90.5 | 101.0 | 121.2 |
| Shear Load, V _{Rd} | [kN] | 8.3 | 12.8 | 19.2 | 35.3 | 55.1 | 79.5 | 103.2 | 125.6 |
| | | | | | Cracked | Concrete | | | |
| Tensile Load, N _{Rd} | [kN] | 9.5 | 13.4 | 16.8 | 25.4 | 28.0 | 41.5 | 55.5 | 66.7 |
| Shear Load, V _{Rd} | [kN] | 8.3 | 12.8 | 19.2 | 35.3 | 55.1 | 79.5 | 103.2 | 125.6 |
| RECOMMENDED LOAD [F _{Rec}] | | | | | | | | | |
| Anchor Size | | M8 | M10 | M12 | M16 | M20 | M24 | M27 | M30 |
| | | | | | Non-Cracke | | | | 50 |
| Tensile Load, N _{Ror} | [kN] | 8.8 | 12.3 | 15.5 | 23.5 | 40.0 | 64.6 | 72.1 | 86.6 |
| Shear Load, V _{Rec} | [kN] | 6.0 | 9.2 | 13.7 | 25.2 | 39.4 | 56.8 | 73.7 | 89.7 |
| · nec | | | l | l | Cracked | Concrete | l | - | l |
| Tensile Load, N _{Rec} | [kN] | 6.8 | 9.5 | 12.0 | 18.2 | 20.0 | 29.6 | 39.7 | 47.6 |
| Shear Load, V _{Rec} | [kN] | 6.0 | 9.2 | 13.7 | 25.2 | 39.4 | 56.8 | 73.7 | 89.7 |

^{*} Bold Italic numbers represent steel failure.



SERVICE TEMPERATURE RANGE

The Statheros EPC80 100% Solid Epoxy Resin performance based on the tabulated temperature range as given below. A gradual temperature increase in base material may lead to a reduction of design bond stress.

| TEMPERATURE RANGE | BASE MATERIAL | MAXIMUM LONG TERM | MAXIMUM SHORT TERM |
|-------------------|-------------------|---------------------------|---------------------------|
| | TEMPERATURE | BASE MATERIAL TEMPERATURE | BASE MATERIAL TEMPERATURE |
| Temperature Range | -40 °C to + 40 °C | + 24 °C | + 40 °C |

Maximum Short Term Base Material Temperature

Short term temperature refers to those elevated base material temperature occurred over brief moment such as diurnal cycling intervals.

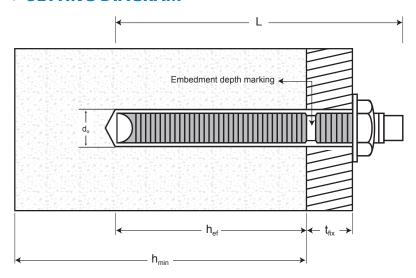
Maximum Long Term Base Material Temperature

Long term temperature refers to those elevated base material temperature occurred over a significant long period of time.

SETTING DETAILS

| ANCHOR SIZE | | M8 | M10 | M12 | M16 | M20 | M24 | M27 | M30 |
|---|------|---------------------|---------------|-------------------------------|-----|-----|---------------------|-----|-----|
| Standard Anchor Length, L | [mm] | 110 | 130 | 160 | 190 | 260 | 300 | 340 | 380 |
| Nominal Drill Hole Diameter, d ₀ | [mm] | 10 | 12 | 14 | 18 | 24 | 28 | 32 | 35 |
| Fixture Hole Diameter, d _{fix} | [mm] | 9 | 12 | 14 | 18 | 22 | 26 | 30 | 33 |
| Maximum Fixture Thickness, t _{fix} | [mm] | 15 | 20 | 30 | 40 | 50 | 55 | 60 | 70 |
| Recommended Torque, T _{inst} | [Nm] | 10 | 20 | 40 | 80 | 135 | 200 | 240 | 270 |
| | | Mir | nimum Anchora | ge Depth, h _{ef,mir} | n | | | | |
| Minimum Anchorage Depth, h _{ef,min} | [mm] | 60 | 60 | 70 | 80 | 90 | 96 | 108 | 120 |
| Minimum Spacing, s _{min} | [mm] | 40 | 40 | 40 | 45 | 50 | 55 | 60 | 65 |
| Minimum Edge Distance, c _{min} | [mm] | 40 | 40 | 40 | 45 | 50 | 55 | 60 | 65 |
| Minimum Concrete Thickness, h _{min} | [mm] | 100 | 100 | 100 | 115 | 130 | 160 | 180 | 200 |
| | | Max | kimum Anchora | ge Depth, h _{ef,ma} | ax | | | | |
| Maximum Anchorage Depth, h _{ef,max} | [mm] | 160 | 200 | 240 | 320 | 400 | 480 | 540 | 600 |
| Minimum Spacing, s _{min} | [mm] | 40 | 40 | 40 | 45 | 50 | 55 | 60 | 65 |
| Minimum Edge Distance, c _{min} | [mm] | 40 | 40 | 40 | 45 | 50 | 55 | 60 | 65 |
| Minimum Concrete Thickness, h _{min} | [mm] | 200 | 224 | 268 | 336 | 444 | 532 | 600 | 670 |
| | | Sta | ndard Anchora | ge Depth, h _{ef,std} | | | | | |
| Standard Anchorage Depth, h _{ef,std} | [mm] | 80 | 90 | 110 | 125 | 170 | 210 | 250 | 270 |
| Minimum Spacing, s _{min} | [mm] | 40 | 45 | 55 | 65 | 85 | 105 | 125 | 135 |
| Minimum Edge Distance, c _{min} | [mm] | 40 | 45 | 55 | 65 | 85 | 105 | 125 | 135 |
| Minimum Concrete Thickness, h _{min} | [mm] | h _{ef,std} | + 30mm ≥ 10 | 0mm | | | $h_{ef,std} + 2d_o$ | | |

SETTING DIAGRAM

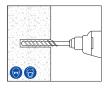




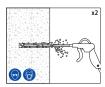
▶ INSTALLATION PROCEDURES

Before commencing installation ensure the operative is equipped with appropriate personal protection equipment, SDS Hammer Drill, Air Blower, Hole Cleaning Brush, good quality Dispensing Tool – either manual or power operated, Chemical Cartridge with mixing nozzle and extension tube, if needed.

 Using the SDS Hammer Drill in rotary hammer mode for drilling, with a carbide tipped drill bit of the appropriate size, drill the hole to the specified hole diameter and depth.

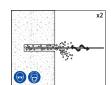


 Insert the Air Lance to the bottom of the hole and depress the trigger for 2 seconds. The compressed air must be clean – free from water and oil – and at a minimum pressure of 6bar.



Perform the blowing operation twice.

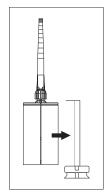
3. Select the correct size Hole Cleaning Brush. Ensure that the brush is in good condition and the correct diameter. Insert the brush to the bottom of the hole, use a brush extension if needed to reach the bottom of the hole and withdraw with a twisting motion. There should be positive interaction between the steel bristles of the brush and the sides of the drilled hole.



Perform the brushing operation twice.

- 4. Repeat 2
- 5. Repeat 3
- 6. Repeat 2
- Select the appropriate static mixer nozzle, check that the mixing elements are present and correct (do not modify the mixer). Attach mixer nozzle to the cartridge. Check the Dispensing Tool is in good working order. Place the cartridge into the dispensing tool.

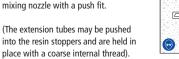
Note: The Nozzle type 4 is in two sections. One section contains the mixing elements and the other section is an extension piece. Connect the extension piece to the mixing section by pushing the two sections firmly together until a positive engagement is felt.

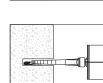


 Extrude some resin to waste until an even-colored mixture is extruded. The cartridge is now ready to use.

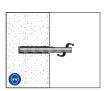


Attach an extension tube with resin stopper (if required) to the end of the mixing nozzle with a push fit.

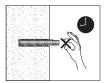




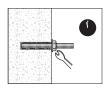
- 10. Insert the mixing nozzle to the bottom of the hole. Extrude the resin and slowly withdraw the nozzle from the hole. Ensure no air voids are created as the nozzle is withdrawn. Inject resin until the hole is approximately ¾ full and remove the nozzle from the hole.
- 11. Select the steel anchor element and ensure it is free from oil or other contaminants, and mark with the required embedment depth. Insert the steel element into the hole using a back and forth twisting motion to ensure complete cover, until it reaches the bottom of the hole. Excess resin will be expelled from the hole evenly around the steel element and there shall be no gaps between the anchor element and the wall of the drilled hole.



- Clean any excess resin from around the mouth of the hole.
- 13. Do not disturb the anchor until at least the minimum curing time has elapsed. Refer to the Gel and Curing Timetable to determine the appropriate cure time.



 Position the fixture and tighten the anchor to the appropriate installation torque.



Do not over-torque the anchor as this could adversely affect its performance.



► GEL AND CURING TIME^{1,2}

| BASE MATERIAL TEMPERATURE T _{base material} (°C) | GEL TIME (WORKING TIME) t _{gel} (mins) | CURING TIME t _{cure} (hrs) |
|--|--|--|
| $+5 \le T_{\text{base material}} < +10$ | 20 | 24 |
| $+10 \le T_{\text{base material}} < +15$ | 20 | 12 |
| $+15 \le T_{\text{base material}} < +20$ | 15 | 8 |
| $+20 \le T_{\text{base material}} < +25$ | 11 | 7 |
| $+25 \le T_{\text{base material}} < +30$ | 8 | 6 |
| $+30 \le T_{\text{base material}} < +35$ | 6 | 5 |
| $+35 \le T_{\text{base material}} < +40$ | 4 | 4 |
| +40 & above | 3 | 3 |

¹ Cartridge should be \ge +10°C.

► MATERIAL SPECIFICATIONS

| DESIGNATION | MATERIAL |
|---------------------------------------|---|
| VA Rods - Class 5.8 & 8.8 M8 - M30 | Strength class 5.8, 8.8 to EN ISO 898-1 Steel, zinc plated \geq 5 μ m to EN ISO 4042 Steel, hot dipped galvanised \geq 40 μ m to EN ISO 10684 |
| Washer ISO 7089 | Steel, zinc plated to EN ISO 4042 Steel, hot dipped galvanised to EN ISO 10684 |
| Hexagon Nut EN ISO 4032 | Strength class 5.8, 8.8 to EN ISO 898-2 Steel galvanised \geq 5 μ m to EN ISO 4042 Hot dipped galvanised \geq 40 μ m to EN ISO 10684 |
| VAS Rods - Class A2 & A4 M8 - M30 | Strength class A2-70 & A4-70 to EN ISO 3506-1 Stainless steel 1.4401; 1.4404; 1.4578; 1.4571; 1.4439; 1.4362 to EN 10088 |
| Washer ISO 7089 | Stainless steel 1.4401; 1.4404; 1.4578; 1.4571; 1.4439; 1.4362 EN 10088 |
| Hexagon Nut EN ISO 4032 | Strength class A2-70 & A4-70 to EN ISO 3506-2 Stainless steel 1.4401; 1.4404; 1.4578; 1.4571; 1.4439; 1.4362 to EN 10088 |

▶ MECHANICAL PROPERTIES

| ANCHOR SIZE | | M8 | M10 | M12 | M16 | M20 | M24 | M27 | M30 |
|---|---------|----------------------|----------------------|----------------------|-------------------------|-------------------------|-------------------------|---------------------------|-----------------------------|
| Cross Sectional Area, A _s | [mm²] | 36.6 | 58.0 | 84.3 | 157.0 | 245.0 | 353.0 | 459.0 | 519.0 |
| Nominal Tensile Strength, f _{uk} ~ Carbon Steel: Class 5.8 ~ High Tensile Steel: Class 8.8 ~ Stainless Steel: Class A2/A4 | [N/mm²] | 500 800 700 | 500 800 700 | 500 800 700 | 500 800 700 | 500 800 700 | 500 800 700 | 500 800 700 | 500 800 700 |
| Nominal Yield Strength, f _{yk} ~ Carbon Steel: Class 5.8 ~ High Tensile Steel: Class 8.8 ~ Stainless Steel: Class A2/A4 | [N/mm²] | 400 640 450 | 400 640 450 | 400 640 450 | 400 640 450 | 400 640 450 | 400 640 450 | 400 640 450 | 400 640 450 |
| Elastic Moment Of Resistance, W _{el} | [mm³] | 31.2 | 62.3 | 109.2 | 277.5 | 540.9 | 935.5 | 1,245.0 | 1,668.0 |
| Design Bending Moment, M _{Rd.s} ~ Carbon Steel: Class 5.8 ~ High Tensile Steel: Class 8.8 ~ Stainless Steel: Class A2/A4 | [Nm] | 15.2 24.0 16.7 | 29.6 48.0 33.3 | 52.8 84.0 59.0 | 132.8 212.8 149.4 | 260.0 415.2 291.0 | 448.8 718.4 503.8 | 665.6 1,065.6 746.8 | 900.0 1,439.2 1,009.0 |

The design bending moment is derived from $M_{Rd,s} = M_{Rd,s}/\gamma_{McN}$ where the partial safety factor is 1.25 for carbon steel 5.8 and high tensile steel 8.8; 1.56 for stainless steel A2/ A4. The recommended bending moment is derived from $M_{Rec,s} = M_{Rd,s}/\gamma_F$ where the partial safety factor is 1.4.



² The curing time are for dry base material only. In wet base material, the curing time must be doubled.

TENSION LOAD [Na.]

Design Tensile Resistance, N_{pd}:

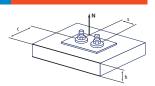
Design Steel Tensile Resistance: Design Pull-Out Resistance: $N_{Rd,s}$

 $N_{Rd,p} = N_{Rd,p}^0 + \Psi_{h,N} + \Psi_{\beta,N}$

lower value of $[N_{Rd,s}; N_{Rd,p}; N_{Rd,c}]$

Design Concrete Cone Resistance:

 $N_{\text{Rd,c}} \; = \; N^{\text{o}}_{\text{Rd,c}} \; , \; \Psi_{\text{h,N}} \; , \; \Psi_{\text{p,N}} \; \; , \; \Psi_{\text{s,N}} \; , \; \Psi_{\text{c,N}} \;$



STEEL TENSILE RESISTANCE [N_{Rd s}]

- For static and quasi-static loadings.
- Only a single anchor is considered.
- For non-cracked and cracked concrete.
- Data valid only for specified steel grade.
- Loading data conformed to ETA-17/0410.



| ANCHOR SIZE | M8 | M10 | M12 | M16 | M20 | M24 | M27 | M30 |
|------------------------|------|---------------|---------------|------|-------|-------|-------|-------|
| | C | arbon Steel: | Class 5.8 | | | | | |
| $N_{Rd,s}$ [kN] | 12.0 | 19.3 | 28.0 | 52.7 | 82.0 | 118.0 | 153.3 | 187.3 |
| | Hig | h Tensile Ste | el: Class 8.8 | | | | | |
| $N_{Rd,s}$ [kN] | 19.3 | 30.7 | 44.7 | 84.0 | 130.7 | 188.0 | 244.7 | 299.3 |
| | Sta | inless Steel: | Class A2/A4 | | | | | |
| N _{Rd,s} [kN] | 13.7 | 21.6 | 31.1 | 57.9 | 90.5 | 130.0 | 168.9 | 206.8 |

The design steel tensile resistance is derived from $N_{Rd,s} = N_{Rk,s} / \gamma_{McN,N}$ where the partial safety factor is 1.5 for carbon steel 5.8 and high tensile steel 8.8; 1.9 for stainless steel A2/A4. The recommended load is derived from $N_{Rec,s} = N_{Rd,s} / \gamma_F$ where the partial safety factor is 1.4.

PULL-OUT RESISTANCE [Npd.]

- For static and quasi-static loadings.
- Only a single anchor is considered.
- No anchor spacing and edge distance influences.
- Loading applicable to dry and wet concrete.
- Concrete compressive strength C20/25 ($f_{ck,cube} = 25 \text{ N/mm}^2$).
- For non-cracked and cracked concrete.
- Loading data conformed to ETA-17/0410.



| ANCHOR SIZE | | M8 | M10 | M12 | M16 | M20 | M24 | M27 | M30 |
|--------------|------|------|-------------|----------|------|------|------|-------|-------|
| $h_{ef,std}$ | [mm] | 80 | 90 | 110 | 125 | 170 | 210 | 250 | 270 |
| | | ٨ | Ion-Cracked | Concrete | | | | | |
| $N_{Rd,p}^0$ | [kN] | 12.3 | 17.3 | 21.7 | 32.9 | 56.0 | 90.5 | 101.0 | 121.2 |
| | | | Cracked Co | ncrete | | | | | |
| $N_{Rd,p}^0$ | [kN] | 9.5 | 13.4 | 16.8 | 25.4 | 28.0 | 41.5 | 55.5 | 66.7 |

The design pull-out resistance is derived from $N_{Rd,p}^0 = N_{Rk,p}^0 / \gamma_{Mc,N}$ where the partial safety factor is 1.8 for M8 ~ M10 and 2.1 for M12 and above. The recommended load is derived from $N_{Rec,p}^0 = N_{Rd,p}^0 / \gamma_F$ where the partial safety factor is 1.4.

CONCRETE CONE RESISTANCE [N_{Rd}c]

- For static and quasi-static loadings.
- Only a single anchor is considered.
- No anchor spacing and edge distance influences.
- Loading applicable to dry and wet concrete.
- Concrete compressive strength C20/25 (f_{ck,cube} = 25 N/mm²).
- For non-cracked and cracked concrete.
- Loading data conformed to ETA-17/0410.



| ANCHOR SIZE | | M8 | M10 | M12 | M16 | M20 | M24 | M27 | M30 | | |
|----------------------|------|------|------|------|------|------|-------|-------|-------|--|--|
| h _{ef,std} | [mm] | 80 | 90 | 110 | 125 | 170 | 210 | 250 | 270 | | |
| Non-Cracked Concrete | | | | | | | | | | | |
| $N^0_{Rd,c}$ | [kN] | 24.1 | 28.7 | 38.8 | 47.1 | 74.6 | 102.5 | 133.1 | 149.4 | | |
| Cracked Concrete | | | | | | | | | | | |
| $N^0_{Rd,c}$ | [kN] | 17.2 | 20.5 | 27.7 | 33.5 | 53.2 | 73.0 | 94.9 | 106.5 | | |

The design concrete cone resistance is derived from $N_{Rd,c}^0 = N_{Rd,c}^0 / \gamma_{RC,c}$ where the partial safety factor is 1.5. The recommended load is derived from $N_{Rec,c}^0 = N_{Rd,c}^0 / \gamma_F$ where the partial safety factor is 1.4.



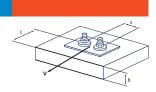
lower value of $[V_{\rm Rd,s}$; $V_{\rm Rd,c}$; $V_{\rm Rd,cp}]$

SHEAR LOAD [V_{pd}]

Design Shear Resistance, V_{Rd}:

Design Steel Shear Resistance:

 $V_{Rd,s}$ Design Concrete Edge Shear Resistance: $V_{Rd,c} = V_{Rd,c}^0 + \Psi_{\beta,V}^* \Psi_{\alpha,V}^* \Psi_{sc,V}$ Design Concrete Pry-Out Resistance: $\boldsymbol{V}_{Rd,cp} = \boldsymbol{V^0}_{Rd,cp} * \boldsymbol{\Psi}_{\boldsymbol{\beta},\boldsymbol{V}^*} \boldsymbol{\Psi}_{\boldsymbol{s},\boldsymbol{N}^*} \boldsymbol{\Psi}_{\boldsymbol{c},\boldsymbol{N}}$



STEEL SHEAR RESISTANCE [V_{Pd c}]

- For static and quasi-static loadings.
- Only a single anchor is considered.
- For non-cracked and cracked concrete.
- Data valid only for specified steel grade.
- Loading data conformed to ETA-17/0410.



| ANCHOR SIZE | M8 | M10 | M12 | M16 | M20 | M24 | M27 | M30 | | | |
|-------------------------------|------|------|------|------|------|-------|-------|-------|--|--|--|
| Carbon Steel: Class 5.8 | | | | | | | | | | | |
| $V_{Rd,s}$ [kN] | 7.2 | 12.0 | 16.8 | 31.2 | 48.8 | 70.4 | 92.0 | 112.0 | | | |
| High Tensile Steel: Class 8.8 | | | | | | | | | | | |
| $V_{Rd,s}$ [kN] | 12.0 | 18.4 | 27.2 | 50.4 | 78.4 | 112.8 | 147.2 | 179.2 | | | |
| Stainless Steel: Class A2/A4 | | | | | | | | | | | |
| $V_{Rd,s}$ [kN] | 8.3 | 12.8 | 19.2 | 35.3 | 55.1 | 79.5 | 103.2 | 125.6 | | | |

The design steel shear resistance is derived from $V_{Rd,s} = V_{Rk,s} / \gamma_{MS,v}$ where the partial safety factor is 1.25 for carbon steel 5.8 and high tensile steel 8.8; 1.56 for stainless steel A2/A4. The recommended load is derived from $V_{\rm Rec,s} = V_{\rm Rd,s}$ / $\gamma_{\rm F}$ where the partial safety factor is 1.4.

CONCRETE EDGE SHEAR RESISTANCE [V_{Rd c}]

- For static and quasi-static loadings.
- Only a single anchor is considered.
- No anchor spacing and edge distance influences.
- Loading applicable to dry and wet concrete.
- Concrete compressive strength C20/25 ($f_{ck,cube} = 25 \text{ N/mm}^2$).
- For non-cracked and cracked concrete.
- Loading data conformed to ETA-17/0410.



| ANCHOR SIZE | | M8 | M10 | M12 | M16 | M20 | M24 | M27 | M30 | | | |
|----------------------|------|-----|-----|-----|------|------|------|------|------|--|--|--|
| h _{ef,std} | [mm] | 80 | 90 | 110 | 125 | 170 | 210 | 250 | 270 | | | |
| C _{min} | [mm] | 40 | 45 | 55 | 65 | 85 | 105 | 125 | 135 | | | |
| Non-Cracked Concrete | | | | | | | | | | | | |
| $V^0_{Rd,c}$ | [kN] | 3.6 | 4.7 | 6.9 | 10.1 | 17.4 | 25.8 | 34.7 | 42.1 | | | |
| Cracked Concrete | | | | | | | | | | | | |
| $V^0_{Rd,c}$ | [kN] | 2.6 | 3.3 | 4.9 | 7.1 | 12.3 | 18.2 | 24.5 | 29.7 | | | |

The design concrete edge shear resistance is derived from $V^0_{Rd,c} = V^0_{Rk,c} \ell_{\gamma_{MCV}}$ where the partial safety factor is 1.5. The recommended load is derived from $V^0_{Rec,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ where the partial safety factor is 1.5. The recommended load is derived from $V^0_{Rec,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ where the partial safety factor is 1.5. The recommended load is derived from $V^0_{Rec,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ where the partial safety factor is 1.5. The recommended load is derived from $V^0_{Rec,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ where the partial safety factor is 1.5. The recommended load is derived from $V^0_{Rec,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ where the partial safety factor is 1.5. The recommended load is derived from $V^0_{Rec,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ where the partial safety factor is 1.5. The recommended load is derived from $V^0_{Rec,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ where the partial safety factor is 1.5. The recommended load is derived from $V^0_{Rec,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ where the partial safety factor is 1.5. The recommended load is derived from $V^0_{Rec,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ where the partial safety factor is 1.5. The recommended load is derived from $V^0_{Rec,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ where $V^0_{Rec,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ is the recommended load is derived from $V^0_{Rd,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ where $V^0_{Rd,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ is the recommended load is derived from $V^0_{Rd,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ where $V^0_{Rd,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ is the recommended load is derived from $V^0_{Rd,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ where $V^0_{Rd,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ is the recommended load is derived from $V^0_{Rd,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ where $V^0_{Rd,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ is the recommended load is derived from $V^0_{Rd,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ where $V^0_{Rd,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ is the $V^0_{Rd,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ where $V^0_{Rd,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ is the $V^0_{Rd,c} = V^0_{Rd,c} \ell_{\gamma_{MCV}}$ where the partial safety factor is 1.4.

CONCRETE PRY-OUT RESISTANCE [V_{Rd.co}]

- For static and quasi-static loadings.
- Only a single anchor is considered.
- No anchor spacing and edge distance influences.
- Loading applicable to dry and wet concrete.
- Concrete compressive strength C20/25 ($f_{ck,cube} = 25 \text{ N/mm}^2$).
- For non-cracked and cracked concrete.
- Loading data conformed to ETA-17/0410.



| ANCHOR SIZE | | M8 | M10 | M12 | M16 | M20 | M24 | M27 | M30 | | | |
|---------------------|----------------------|------|------|------|------|-------|-------|-------|-------|--|--|--|
| h _{ef,std} | [mm] | 80 | 90 | 110 | 125 | 170 | 210 | 250 | 270 | | | |
| | Non-Cracked Concrete | | | | | | | | | | | |
| $V_{Rd,cp}^0$ | [kN] | 48.2 | 57.5 | 77.7 | 94.1 | 149.2 | 204.9 | 266.2 | 298.7 | | | |
| Cracked Concrete | | | | | | | | | | | | |
| $V^0_{Rd,cp}$ | [kN] | 34.3 | 41.0 | 55.4 | 67.1 | 106.4 | 146.1 | 189.7 | 213.0 | | | |

The design concrete pry-out resistance is derived from $V^0_{Rd,p} = V^0_{Rk,p}/\gamma_{Mp,\nu}$ where the partial safety factor is 1.5. The recommended load is derived from $V^0_{Rec,p} = V^0_{Rd,p}/\gamma_F$ where the partial safety factor is 1.4.

COMBINED TENSION & SHEAR

Combined Tension & Shear:
$$\frac{N_{sd}}{N_{cl}} + \frac{V_{sd}}{V_{cl}} \le 1.3$$

The resultant force must be satisfied to the above conditions. The designer must cross check the loading conditions, types of applied loads and substrate to ensure the recommended anchor is applicable to the actual site applications. This would avoid any design faults which commonly caused by inconclusive load requirements with respective to actual site conditions.



► INFLUENCING FACTORS - TENSION

INFLUENCE OF ANCHORAGE DEPTH $[\Psi_{b,N}]$

$$\psi_{h,N} = \frac{h_{act}}{h_{efstd}}$$

Limits:
$$h_{ef,min} \leq h_{act} \leq$$
 20 * d

INFLUENCE OF CONCRETE STRENGTH ON PULL-OUT AND CONCRETE CONE RESISTANCE $[\Psi_{g,n}]$

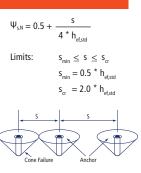
$$\psi_{\beta,N} = \left(\frac{f_{ck,cube}}{25} \right)^{0}.$$

$$\psi_{\text{p,N}} = \; (\frac{f_{\text{d,cube}}}{25})^{\quad \ \, 0.3} \qquad \qquad \text{Limits: 25 MPa} \; \leq \; f_{\text{d,cube}} \; \leq \; 60 \; \text{MPa}$$

| Concrete Strength Designation (ENV 206) | | C 20/25 | C 25/30 | C 30/37 | C 35/45 | C 40/50 | C 50/60 |
|---|-------|---------|---------|---------|---------|---------|---------|
| Concrete Cylinder Strength, f _{ck,cyl} | [MPa] | 20 | 25 | 30 | 35 | 40 | 50 |
| Concrete Cube Strength, f _{ck,cube} | [MPa] | 25 | 30 | 37 | 45 | 50 | 60 |
| Concrete Strength Factor, $\psi_{\beta,N}$ | | 1.00 | 1.06 | 1.12 | 1.19 | 1.23 | 1.30 |

INFLUENCE OF ANCHOR SPACING [Ψ, ,,]

| | S,N- | | | | | | | |
|--|------|------|------|------|------|------|------|------|
| Anchor Spacing 's' [mm] | M8 | M10 | M12 | M16 | M20 | M24 | M27 | M30 |
| 40 | 0.63 | | | | | | | |
| 45 | 0.64 | 0.63 | | | | | | |
| 55 | 0.67 | 0.65 | 0.63 | | | | | |
| 65 | 0.70 | 0.68 | 0.65 | 0.63 | | | | |
| 85 | 0.77 | 0.74 | 0.69 | 0.67 | 0.63 | | | |
| 105 | 0.83 | 0.79 | 0.74 | 0.71 | 0.65 | 0.63 | | |
| 125 | 0.89 | 0.85 | 0.78 | 0.75 | 0.68 | 0.65 | 0.63 | |
| 135 | 0.92 | 0.88 | 0.81 | 0.77 | 0.70 | 0.66 | 0.64 | 0.63 |
| 160 | 1.00 | 0.94 | 0.86 | 0.82 | 0.74 | 0.69 | 0.66 | 0.65 |
| 180 | | 1.00 | 0.91 | 0.86 | 0.76 | 0.71 | 0.68 | 0.67 |
| 220 | | | 1.00 | 0.94 | 0.82 | 0.76 | 0.72 | 0.70 |
| 250 | | | | 1.00 | 0.87 | 0.80 | 0.75 | 0.73 |
| 340 | | | | | 1.00 | 0.90 | 0.84 | 0.81 |
| 420 | | | | | | 1.00 | 0.92 | 0.89 |
| 500 | | | | | | | 1.00 | 0.96 |
| 540 | | | | | | | | 1.00 |
| Critical Spacing 's _{cr} ' [mm] | 160 | 180 | 220 | 250 | 340 | 420 | 500 | 540 |
| Minimum Spacing 's _{min} ' [mm] | 40 | 45 | 55 | 65 | 85 | 105 | 125 | 135 |

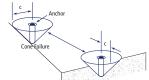


INFLUENCE OF EDGE DISTANCE $[\psi_{c,N}]$

| Edge Distance 'c' [mm] | M8 | M10 | M12 | M16 | M20 | M24 | M27 | M30 |
|--|------|------|------|------|------|------|------|------|
| 40 | 0.65 | | | | | | | |
| 45 | 0.69 | 0.65 | | | | | | |
| 55 | 0.78 | 0.73 | 0.65 | | | | | |
| 65 | 0.87 | 0.81 | 0.71 | 0.66 | | | | |
| 80 | 1.00 | 0.92 | 0.81 | 0.75 | | | | |
| 85 | | 0.96 | 0.84 | 0.78 | 0.65 | | | |
| 90 | | 1.00 | 0.87 | 0.80 | 0.67 | | | |
| 105 | | | 0.97 | 0.89 | 0.73 | 0.65 | | |
| 110 | | | 1.00 | 0.92 | 0.75 | 0.67 | | |
| 125 | | | | 1.00 | 0.81 | 0.72 | 0.65 | |
| 135 | | | | | 0.86 | 0.75 | 0.68 | 0.65 |
| 150 | | | | | 0.92 | 0.80 | 0.72 | 0.69 |
| 165 | | | | | 0.98 | 0.85 | 0.76 | 0.73 |
| 170 | | | | | 1.00 | 0.87 | 0.78 | 0.74 |
| 210 | | | | | | 1.00 | 0.89 | 0.84 |
| 250 | | | | | | | 1.00 | 0.95 |
| 270 | | | | | | | | 1.00 |
| Critical Edge Distance ' c_{α} ' [mm] | 80 | 90 | 110 | 125 | 170 | 210 | 250 | 270 |
| Minimum Edge Distance 'c _{min} ' [mm] | 40 | 45 | 55 | 65 | 85 | 105 | 125 | 135 |



 $c_{min} = 0.5 * h_{ef,std}$ $c_{cr} = 1.0 * h_{ef,std}$





► INFLUENCING FACTORS - SHEAR

INFLUENCE OF CONCRETE STRENGTH ON CONCRETE EDGE SHEAR AND CONCRETE PRY-OUT RESISTANCE $[\Psi_{B,V}]$

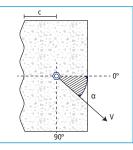
$$\psi_{\beta,V} = \sqrt{\frac{f_{ck,cube}}{25}}$$

Limits: 25 MPa $\leq f_{dk,cube} \leq$ 60 MPa

| Concrete Strength Designation (ENV 206) | | C 20/25 | C 25/30 | C 30/37 | C 35/45 | C 40/50 | C 50/60 |
|---|-------|---------|---------|---------|---------|---------|---------|
| Concrete Cylinder Strength, f _{ck,cyl} | [MPa] | 20 | 25 | 30 | 35 | 40 | 50 |
| Concrete Cube Strength, f _{ck,cube} | [MPa] | 25 | 30 | 37 | 45 | 50 | 60 |
| Concrete Strength Factor, $\psi_{\beta,V}$ | | 1.00 | 1.10 | 1.22 | 1.34 | 1.41 | 1.55 |

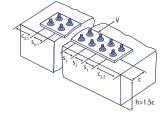
INFLUENCE OF SHEAR LOAD DIRECTION $[\Psi_{\alpha \nu}]$

| Load Type | Angle, α [°] | $\Psi_{a,v}$ |
|-------------|-------------------|--------------|
| Oblique 0° | 0° < α ≤ 15° | 1.00 |
| Oblique 30° | 15° < α ≤ 37.5° | 1.14 |
| Oblique 45° | 37.5° < α ≤ 52.5° | 1.35 |
| Oblique 60° | 52.5° < α ≤ 67.5° | 1.71 |
| Oblique 90° | 67.5° < α ≤ 90° | 2.00 |



INFLUENCE OF ANCHOR SPACING AND EDGE DISTANCE ON CONCRETE EDGE SHEAR RESISTANCE $[\Psi_{sc,v}]$

$$\begin{split} &\psi_{sc,V} = \frac{c}{c_{min}} \ \ * \ \, \sqrt{\frac{c}{c_{min}}} & \text{for single anchor towards a concrete edge} \\ &\psi_{sc,V} = \frac{3c+s}{6c_{min}} \ \ * \ \, \sqrt{\frac{c}{c_{min}}} & \text{for two anchors when } s \leq 3c \\ &\psi_{sc,V} = \frac{3c+s_1+s_2+s_{n-1}}{3nc_{min}} \ \ \ * \ \, \sqrt{\frac{c}{c_{min}}} & \text{for multiple anchors when } s_1 \text{ to } s_{n-1} \leq 3c \text{ and } c_2 \geq 1.5c \end{split}$$



| | | | c/c _{min} | | | | | | | | | | | | | | |
|----------------------|----------------------|------|--------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| Ų | $\mu_{\sf sc,V}$ | 1.0 | 1.2 | 1.4 | 1.6 | 1.8 | 2.0 | 2.2 | 2.4 | 2.6 | 2.8 | 3.0 | 3.2 | 3.4 | 3.6 | 3.8 | 4.0 |
| Edge influ single | ience with anchor | 1.00 | 1.31 | 1.66 | 2.02 | 2.41 | 2.83 | 3.26 | 3.72 | 4.19 | 4.69 | 5.20 | 5.72 | 6.27 | 6.83 | 7.41 | 8.00 |
| | 1.0 | 0.67 | 0.84 | 1.03 | 1.22 | 1.43 | 1.65 | 1.88 | 2.12 | 2.36 | 2.62 | 2.89 | 3.16 | 3.44 | 3.73 | 4.03 | 4.33 |
| | 1.5 | 0.75 | 0.93 | 1.12 | 1.33 | 1.54 | 1.77 | 2.00 | 2.25 | 2.50 | 2.76 | 3.03 | 3.31 | 3.60 | 3.89 | 4.19 | 4.50 |
| | 2.0 | 0.83 | 1.02 | 1.22 | 1.43 | 1.65 | 1.89 | 2.13 | 2.38 | 2.63 | 2.90 | 3.18 | 3.46 | 3.75 | 4.05 | 4.35 | 4.67 |
| | 2.5 | 0.92 | 1.11 | 1.32 | 1.54 | 1.77 | 2.00 | 2.25 | 2.50 | 2.77 | 3.04 | 3.32 | 3.61 | 3.90 | 4.21 | 4.52 | 4.83 |
| | 3.0 | 1.00 | 1.20 | 1.42 | 1.64 | 1.88 | 2.12 | 2.37 | 2.63 | 2.90 | 3.18 | 3.46 | 3.76 | 4.06 | 4.36 | 4.68 | 5.00 |
| | 3.5 | | 1.30 | 1.52 | 1.75 | 1.99 | 2.24 | 2.50 | 2.76 | 3.04 | 3.32 | 3.61 | 3.91 | 4.21 | 4.52 | 4.84 | 5.17 |
| | 4.0 | | | 1.62 | 1.86 | 2.10 | 2.36 | 2.62 | 2.89 | 3.17 | 3.46 | 3.75 | 4.05 | 4.36 | 4.68 | 5.00 | 5.33 |
| | 4.5 | | | | 1.96 | 2.21 | 2.47 | 2.74 | 3.02 | 3.31 | 3.60 | 3.90 | 4.20 | 4.52 | 4.84 | 5.17 | 5.50 |
| | 5.0 | | | | | 2.33 | 2.59 | 2.87 | 3.15 | 3.44 | 3.74 | 4.04 | 4.35 | 4.67 | 5.00 | 5.33 | 5.67 |
| | 5.5 | | | | | | 2.71 | 2.99 | 3.28 | 3.57 | 3.88 | 4.19 | 4.50 | 4.82 | 5.15 | 5.49 | 5.83 |
| | 6.0 | | | | | | 2.83 | 3.11 | 3.41 | 3.71 | 4.02 | 4.33 | 4.65 | 4.98 | 5.31 | 5.65 | 6.00 |
| s/c _{min} | 6.5 | | | | | | | 3.24 | 3.53 | 3.84 | 4.16 | 4.47 | 4.80 | 5.13 | 5.47 | 5.82 | 6.17 |
| | 7.0 | | | | | | | | 3.67 | 3.98 | 4.29 | 4.62 | 4.95 | 5.29 | 5.63 | 5.98 | 6.33 |
| | 7.5 | | | | | | | | | 4.11 | 4.43 | 4.76 | 5.10 | 5.44 | 5.79 | 6.14 | 6.50 |
| | 8.0 | | | | | | | | | | 4.57 | 4.91 | 5.25 | 5.59 | 5.95 | 6.30 | 6.67 |
| | 8.5 | | | | | | | | | | | 5.05 | 5.40 | 5.75 | 6.10 | 6.47 | 6.83 |
| | 9.0 | | | | | | | | | | | 5.20 | 5.55 | 5.90 | 6.26 | 6.63 | 7.00 |
| | 9.5 | | | | | | | | | | | | 5.69 | 6.05 | 6.42 | 6.79 | 7.17 |
| | 10.0 | | | | | | | | | | | | | 6.21 | 6.58 | 6.95 | 7.33 |
| | 10.5 | | | | | | | | | | | | | | 6.74 | 7.12 | 7.50 |
| | 11.0 | | | | | | | | | | | | | | | 7.28 | 7.67 |
| | 11.5 | | | | | | | | | | | | | | | | 7.83 |
| | 12.0 | | | | | | | | | | | | | | | | 8.00 |

(Design Load Approach with BS8110 Bond Strength Method)

Concrete Compressive Strength: f_{ck.cube} = 25 N/mm²

| Rebar Size, d _s | | ф10 | ф12 | ф16 | ф20 | ф25 | ф32 | ф40 |
|---|----------------------|---------|---------|---------------|-----------------|----------------------------|----------------|---------|
| Design Steel Resistance, N _{Rd,s} | [kN] | 31.4 | 45.2 | 80.4 | 125.7 | 196.4 | 321.7 | 502.7 |
| Design Bond Stress, $	au_{_{Rd}}$ | [N/mm ²] | 6.1 | 5.2 | 5.7 | 5.7 | 5.7 | 5.7 | 5.2 |
| Drilled Hole Diameter, d _o | [mm] | 13 ~ 14 | 15 ~ 16 | 20 ~ 22 | 25 ~ 28 | 30 ~ 32 | 40 ~ 42 | 50 ~ 52 |
| Bar Spacing, s | [mm] | 50 | 65 | 80 | 100 | 125 | 160 | 200 |
| Edge Distance, c | [mm] | 40 | 40 | 40 | 50 | 65 | 80 | 100 |
| L _{b,rqd} / Rebar φ | | 16 | 19 | 18 | 18 | 18 | 18 | 19 |
| Anchorage Length, L _b [mm] | | | | Design Tensil | le Bonding Capa | city, N _{Rd} [kN] | | |
| 100 | | 19.2 | | | | | | |
| 120 | | 23.0 | 23.7 | | | "Minimum de | pth to develop | |
| 160 | | 30.7 | 31.6 | 46.0 | | full stee | el shear" | |
| 200 | | 31.4 | 39.5 | 57.5 | 71.8 | | | |
| 250 | | | 45.2 | 71.8 | 89.8 | 112.2 | | |
| 320 | | | | 80.4 | 114.9 | 143.6 | 183.9 | |
| 350 | | | | | 125.7 | 157.1 | 201.1 | |
| 400 | | | | | | 179.5 | 229.8 | 263.3 |
| 440 | | | | | | 196.4 | 252.8 | 289.7 |
| 500 | | | | | | | 287.3 | 329.2 |
| 560 | | | | | | | 321.7 | 368.7 |
| 650 | | | | | | | | 427.9 |
| 700 | | | | | | | | 460.8 |
| 770 | | | | | | | | 502.7 |
| Length to Develop Steel Yield, L _{b,rqd} [mm |] | 164 | 229 | 280 | 350 | 438 | 560 | 764 |

- Safety factor for design tensile steel resistance: γ_{Mc,N} = 1.15 (based on steel yield strength of 460 N/mm²).
 Safety factor for design tensile pull-out resistance: γ_{Mc,N} = 1.8 for φ10 and 2.1 for φ12 and above.
 Loading applicable to non-cracked concrete with design comply in accordance to BS8110.
 Loading data conformed to ETA-17/0410 ETAG 001 Part 1 & Part 5 Option 1.
 Safety factor for design tensile concrete cone resistance: γ_{Mc,N} = 1.5
 Minimum spacing shall be 4d_s bar to bar or 5d_s centre-to-centre.
 Minimum edge distance shall be 2d_s bar to bar or 2.5d_s centre-to-centre.

APPROVAL LISTING





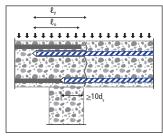


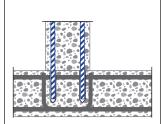


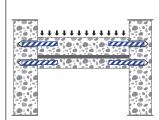


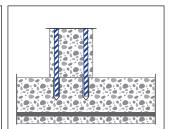


SUGGESTED APPLICATIONS









Overlap joints for slabs and beams or foundation column or wall; rebar connection for simply supported slabs or beams; shear connector or compression component joints.



(Design Load Approach with BS8110 Bond Strength Method)

Concrete Compressive Strength: f_{ck.cube} = 30 N/mm²

| Rebar Size, d _s | | ф10 | ф12 | ф16 | ф20 | ф25 | ф32 | ф40 |
|--|----------------------|---------|---------|---------------|----------------|----------------------------|----------------|---------|
| Design Steel Resistance, N _{Rd,s} | [kN] | 31.4 | 45.2 | 80.4 | 125.7 | 196.4 | 321.7 | 502.7 |
| Design Bond Stress, $	au_{	ext{Rd}}$ | [N/mm ²] | 6.3 | 5.4 | 5.9 | 5.9 | 5.9 | 5.9 | 5.4 |
| Drilled Hole Diameter, d _o | [mm] | 13 ~ 14 | 15 ~ 16 | 20 ~ 22 | 25 ~ 28 | 30 ~ 32 | 40 ~ 42 | 50 ~ 52 |
| Bar Spacing, s | [mm] | 50 | 65 | 80 | 100 | 125 | 160 | 200 |
| Edge Distance, c | [mm] | 40 | 40 | 40 | 50 | 65 | 80 | 100 |
| L _{b,rqd} / Rebar φ | | 16 | 19 | 17 | 17 | 17 | 17 | 19 |
| Anchorage Length, L _b [mm] | | | | Design Tensil | e Bonding Capa | city, N _{Rd} [kN] | | |
| 100 | | 19.8 | | | | | | |
| 120 | | 23.7 | 24.4 | | | "Minimum de | pth to develop | |
| 160 | | 31.4 | 32.5 | 47.3 | | full stee | el shear" | |
| 200 | | | 40.7 | 59.2 | 74.0 | | | |
| 225 | | | 45.2 | 66.6 | 83.2 | | | |
| 250 | | | | 74.0 | 92.5 | 115.6 | | |
| 275 | | | | 80.4 | 101.7 | 127.1 | | |
| 320 | | | | | 118.4 | 147.9 | 189.4 | |
| 340 | | | | | 125.7 | 157.2 | 201.2 | |
| 400 | | | | | | 184.9 | 236.7 | 271.2 |
| 425 | | | | | | 196.4 | 251.5 | 288.2 |
| 475 | | | | | | | 281.1 | 322.1 |
| 545 | | | | | | | 321.7 | 369.6 |
| 600 | | | | | | | | 406.8 |
| 740 | | | | | | | | 502.7 |
| Length to Develop Steel Yield, L _{b,rqd} [mm] | | 159 | 222 | 272 | 340 | 425 | 544 | 741 |

- Safety factor for design tensile steel resistance: γ_{Ms,N} = 1.15 (based on steel yield strength of 460 N/mm²).
 Safety factor for design tensile pull-out resistance: γ_{Mc,N} = 1.8 for φ10 and 2.1 for φ12 and above.
 Loading applicable to non-cracked concrete with design comply in accordance to BS8110.

- 4) Loading data conformed to ETA-17/0410 ETAG 001 Part 1 & Part 5 Option 1.
- 5) Safety factor for design tensile concrete cone resistance: $\gamma_{Mc,N}=1.5$ Minimum spacing shall be $4d_s$ bar to bar or $5d_s$ centre-to-centre.
- 7) Minimum edge distance shall be 2d_s bar to bar or 2.5d_s centre-to-centre.

APPROVAL LISTING





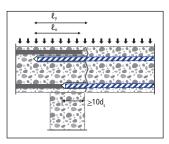


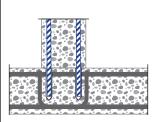


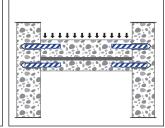


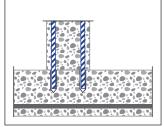


SUGGESTED APPLICATIONS









Overlap joints for slabs and beams or foundation column or wall; rebar connection for simply supported slabs or beams; shear connector or compression component joints.



(Design Load Approach with BS8110 Bond Strength Method)

Concrete Compressive Strength: f_{ck.cube} = 35 N/mm²

| Rebar Size, d _s | | ф10 | ф12 | ф16 | ф20 | ф25 | ф32 | ф40 | |
|--|----------------------|---|---------|---------|---------|---------------------------|---------|---------|--|
| Design Steel Resistance, N _{Rd,s} | [kN] | 31.4 | 45.2 | 80.4 | 125.7 | 196.4 | 321.7 | 502.7 | |
| Design Bond Stress, $	au_{_{Rd}}$ | [N/mm ²] | 6.4 | 5.5 | 6.0 | 6.0 | 6.0 | 6.0 | 5.5 | |
| Drilled Hole Diameter, d _o | [mm] | 13 ~ 14 | 15 ~ 16 | 20 ~ 22 | 25 ~ 28 | 30 ~ 32 | 40 ~ 42 | 50 ~ 52 | |
| Bar Spacing, s | [mm] | 50 | 65 | 80 | 100 | 125 | 160 | 200 | |
| Edge Distance, c | [mm] | 40 | 40 | 40 | 50 | 65 | 80 | 100 | |
| L _{b,rqd} / Rebar φ | | 16 | 18 | 17 | 17 | 17 | 17 | 18 | |
| Anchorage Length, L _b [mm] | | Design Tensile Bonding Capacity, N _{Rd} [kN] | | | | | | | |
| 100 | | 20.2 | | | | | | | |
| 120 | | 24.2 | 24.9 | | | | | | |
| 160 | | 31.4 | 33.2 | 48.3 | | "Minimum depth to develop | | | |
| 200 | | | 41.5 | 60.3 | 75.4 | full steel shear" | | | |
| 220 | | | 45.2 | 66.4 | 82.9 | | | | |
| 250 | | | | 75.4 | 94.3 | 117.8 | | | |
| 265 | | | | 80.4 | 99.9 | 124.9 | | | |
| 300 | | | | | 113.1 | 141.4 | | | |
| 320 | | | | | 125.7 | 150.8 | 193.0 | | |
| 375 | | | | | | 176.7 | 226.2 | | |
| 400 | | | | | | 196.4 | 241.3 | 276.5 | |
| 450 | | | | | | | 271.5 | 311.1 | |
| 535 | | | | | | | 321.7 | 369.8 | |
| 600 | | | | | | | | 414.7 | |
| 725 | | | | | | | | 502.7 | |
| Length to Develop Steel Yield, L _{b,rqd} [mm] | | 156 | 218 | 267 | 333 | 417 | 533 | 727 | |

- Safety factor for design tensile steel resistance: γ_{Ms,N} = 1.15 (based on steel yield strength of 460 N/mm²).
 Safety factor for design tensile pull-out resistance: γ_{Mc,N} = 1.8 for φ10 and 2.1 for φ12 and above.
 Loading applicable to non-cracked concrete with design comply in accordance to BS8110.

- 4) Loading data conformed to ETA-17/0410 ETAG 001 Part 1 & Part 5 Option 1.
- 5) Safety factor for design tensile concrete cone resistance: $\gamma_{Mc,N}=1.5$ Minimum spacing shall be $4d_s$ bar to bar or $5d_s$ centre-to-centre.
- 7) Minimum edge distance shall be 2d_s bar to bar or 2.5d_s centre-to-centre.

APPROVAL LISTING





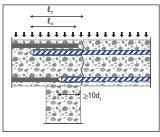


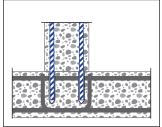


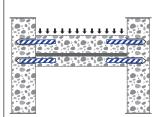


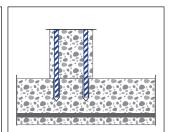


SUGGESTED APPLICATIONS









Overlap joints for slabs and beams or foundation column or wall; rebar connection for simply supported slabs or beams; shear connector or compression component joints.



(Design Load Approach with BS8110 & ACI 318 Concrete Splitting Criteria)

Concrete Compressive Strength: f_{ck.cube} = 25 N/mm²

| Rebar Size, d _s | | ф10 | ф12 | ф16 | ф20 | ф25 | ф32 | ф40 | |
|---|----------------------|---------|---------|-------------------|------------------|-------------------------------|-------------------|---------|--|
| Design Steel Resistance, N _{Rd,s} | [kN] | 34.4 | 49.6 | 88.1 | 137.6 | 215.1 | 352.4 | 550.6 | |
| Splitting Bond Stress, $	au_{	ext{sp,d}}$ | [N/mm ²] | 3.49 | 3.49 | 3.49 | 3.25 | 2.80 | 2.80 | 2.80 | |
| Drilled Hole Diameter, d _o | [mm] | 13 ~ 14 | 15 ~ 16 | 20 ~ 22 | 25 ~ 28 | 30 ~ 32 | 40 ~ 42 | 50 ~ 52 | |
| Bar Spacing, s | [mm] | 50 | 60 | 80 | 100 | 125 | 160 | 200 | |
| Edge Distance, c | [mm] | 40 | 40 | 40 | 50 | 65 | 80 | 100 | |
| L _{b,rqd} / Rebar φ | | 31 | 31 | 31 | 34 | 39 | 39 | 39 | |
| Anchorage Length, L _b [mm] | | | Desig | n Tensile Pull-Ou | t / Concrete Cor | ne Resistance, N _R | _d [kN] | | |
| 100 | | 11.0 | | | | | | | |
| 120 | | 13.2 | 15.8 | | " | Minimum dept | | ıll | |
| 160 | | 17.5 | 21.1 | 28.1 | | steel shear" | | | |
| 200 | | 21.9 | 26.3 | 35.1 | 40.8 | | | | |
| 250 | | 27.4 | 32.9 | 43.9 | 51.1 | 55.0 | | | |
| 300 | | 32.9 | 39.5 | 52.6 | 61.3 | 66.0 | | | |
| 320 | | 34.4 | 42.1 | 56.1 | 65.4 | 70.4 | 90.1 | | |
| 400 | | | 49.6 | 70.2 | 81.7 | 88.0 | 112.6 | 140.8 | |
| 450 | | | | 79.0 | 91.9 | 99.0 | 126.7 | 158.4 | |
| 500 | | | | 88.1 | 102.1 | 110.0 | 140.8 | 176.0 | |
| 600 | | | | | 122.5 | 132.0 | 168.9 | 211.1 | |
| 675 | | | | | 137.6 | 148.5 | 190.0 | 237.5 | |
| 750 | | | | | | 165.0 | 211.1 | 263.9 | |
| 980 | | | | | | 215.1 | 275.9 | 344.9 | |
| 1000 | | | | | | | 281.5 | 351.9 | |
| 1250 | | | | | | | 352.4 | 439.9 | |
| 1400 | | | | | | | | 492.7 | |
| 1565 | | | | | | | | 550.6 | |
| Length to Develop Steel Yield, $L_{b,rqd}$ [mm] | | 314 | 377 | 502 | 674 | 978 | 1,252 | 1,565 | |

- 1) Design tensile steel resistance: $N_{\text{Nd,S}} = f_y * A_s / \gamma_{Ms,N}$ where $\gamma_{Ms,N} = 1.05$ (based on steel yield of 460 N/mm²). 2) Design value complied in accordance to BS8110 and ACI 318 concrete splitting criteria.
- 3) Loading data conformed to ETA-17/0410 ETAG 001 Part 1 & Part 5 Option 1.
- Minimum spacing shall be 4d₂ bar to bar or 5d₂ centre-to-centre.
- 5) Minimum edge distance shall be 2d bar to bar or 2.5d centre-to-centre.
- 6) Applicable to dry and wet concrete application.
- 7) Design value based on non-cracked concrete.

APPROVAL LISTING





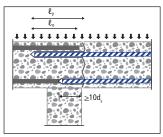


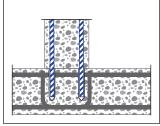


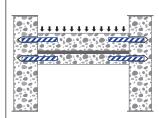


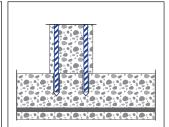


SUGGESTED APPLICATIONS









Overlap joints for slabs and beams or foundation column or wall; rebar connection for simply supported slabs or beams; shear connector or compression component joints.



(Design Load Approach with BS8110 & ACI 318 Concrete Splitting Criteria)

Concrete Compressive Strength: f_{ck.cube} = 30 N/mm²

| Rebar Size, d _s | | ф10 | ф12 | ф16 | ф20 | ф25 | ф32 | ф40 |
|--|----------------------|--|---------|---------|---------|--------------|-----------------|---------|
| Design Steel Resistance, N _{Rd,s} | [kN] | 34.4 | 49.6 | 88.1 | 137.6 | 215.1 | 352.4 | 550.6 |
| Splitting Bond Stress, $	au_{	ext{sp,d}}$ | [N/mm ²] | 3.91 | 3.91 | 3.91 | 3.63 | 3.13 | 3.13 | 3.13 |
| Drilled Hole Diameter, d _o | [mm] | 13 ~ 14 | 15 ~ 16 | 20 ~ 22 | 25 ~ 28 | 30 ~ 32 | 40 ~ 42 | 50 ~ 52 |
| Bar Spacing, s | [mm] | 50 | 60 | 80 | 100 | 125 | 160 | 200 |
| Edge Distance, c | [mm] | 40 | 40 | 40 | 50 | 65 | 80 | 100 |
| L _{b,rqd} / Rebar φ | | 28 | 28 | 28 | 30 | 35 | 35 | 35 |
| Anchorage Length, L _b [mm] | | Design Tensile Pull-Out / Concrete Cone Resistance, N _{Rd} [kN] | | | | | kd [kN] | |
| 100 | | 12.3 | | | | | | |
| 120 | | 14.7 | 17.7 | | " | | h to develop fo | ull |
| 160 | | 19.7 | 23.6 | 31.5 | | steel shear" | | |
| 200 | | 24.6 | 29.5 | 39.3 | 45.6 | | | |
| 250 | | 30.7 | 36.9 | 49.1 | 57.0 | 61.5 | | |
| 275 | | 33.8 | 40.5 | 54.1 | 62.7 | 67.6 | | |
| 280 | | 34.4 | 41.3 | 55.0 | 63.9 | 68.8 | | |
| 320 | | | 47.2 | 62.9 | 73.0 | 78.7 | 100.7 | |
| 335 | | | 49.6 | 65.8 | 76.4 | 82.4 | 105.4 | |
| 400 | | | | 78.6 | 91.2 | 98.3 | 125.9 | 157.4 |
| 450 | | | | 88.1 | 102.6 | 110.6 | 141.6 | 177.0 |
| 525 | | | | | 119.8 | 129.1 | 165.2 | 206.5 |
| 605 | | | | | 137.6 | 148.7 | 190.4 | 238.0 |
| 750 | | | | | | 184.4 | 236.0 | 295.0 |
| 875 | | | | | | 215.1 | 275.4 | 344.2 |
| 950 | | | | | | | 299.0 | 373.7 |
| 1120 | | | | | | | 352.4 | 440.6 |
| 1300 | | | | | | | | 511.4 |
| 1400 | | | | | | | | 550.6 |
| Length to Develop Steel Yield, L _{b,rqd} [mm] | | 280 | 336 | 448 | 603 | 875 | 1,120 | 1,400 |

- 1) Design tensile steel resistance: $N_{Rd,s} = f_y * A_s / \gamma_{Ms,N}$ where $\gamma_{Ms,N} = 1.05$ (based on steel yield of 460 N/mm²). 2) Design value complied in accordance to BS8110 and ACI 318 concrete splitting criteria.
- 3) Loading data conformed to ETA-17/0410 ETAG 001 Part 1 & Part 5 Option 1.
- 4) Minimum spacing shall be 4d₂ bar to bar or 5d₂ centre-to-centre.
- Minimum edge distance shall be 2d_c bar to bar or 2.5d_c centre-to-centre.
- 6) Applicable to dry and wet concrete application.
- 7) Design value based on non-cracked concrete.

APPROVAL LISTING





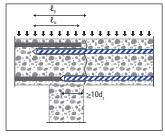


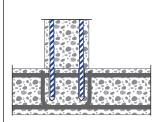


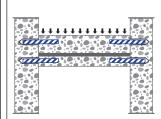


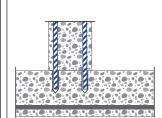


SUGGESTED APPLICATIONS









Overlap joints for slabs and beams or foundation column or wall; rebar connection for simply supported slabs or beams; shear connector or compression component joints.



(Design Load Approach with BS8110 & ACI 318 Concrete Splitting Criteria)

Concrete Compressive Strength: f_{ck.cube} = 35 N/mm²

| Rebar Size, d _s | | ф10 | ф12 | ф16 | ф20 | ф25 | ф32 | ф40 |
|--|----------------------|--|---------|---------|---------|--------------|-----------------|---------|
| Design Steel Resistance, N _{Rd,s} | [kN] | 34.4 | 49.6 | 88.1 | 137.6 | 215.1 | 352.4 | 550.6 |
| Splitting Bond Stress, $	au_{	ext{sp,d}}$ | [N/mm ²] | 4.17 | 4.17 | 4.17 | 3.88 | 3.34 | 3.34 | 3.34 |
| Drilled Hole Diameter, d _o | [mm] | 13 ~ 14 | 15 ~ 16 | 20 ~ 22 | 25 ~ 28 | 30 ~ 32 | 40 ~ 42 | 50 ~ 52 |
| Bar Spacing, s | [mm] | 50 | 60 | 80 | 100 | 125 | 160 | 200 |
| Edge Distance, c | [mm] | 40 | 40 | 40 | 50 | 65 | 80 | 100 |
| L _{b,rqd} / Rebar φ | | 26 | 26 | 26 | 28 | 33 | 33 | 33 |
| Anchorage Length, L _b [mm] | | Design Tensile Pull-Out / Concrete Cone Resistance, N _{Rd} [kN] | | | | | kN] | |
| 100 | | 13.1 | | | | | | |
| 120 | | 15.7 | 18.9 | | " | | h to develop fu | ıll |
| 160 | | 21.0 | 25.2 | 33.5 | | steel shear" | | |
| 200 | | 26.2 | 31.4 | 41.9 | 48.8 | | | |
| 250 | | 32.8 | 39.3 | 52.4 | 61.0 | 65.6 | | |
| 265 | | 34.4 | 41.7 | 55.6 | 64.6 | 69.5 | | |
| 300 | | | 47.2 | 62.9 | 73.1 | 78.7 | | |
| 320 | | | 49.6 | 67.1 | 78.0 | 84.0 | 107.5 | |
| 375 | | | | 78.6 | 91.4 | 98.4 | 125.9 | |
| 400 | | | | 88.1 | 97.5 | 104.9 | 134.3 | 167.9 |
| 450 | | | | | 109.7 | 118.1 | 151.1 | 188.9 |
| 565 | | | | | 137.6 | 148.2 | 189.7 | 237.2 |
| 700 | | | | | | 183.6 | 235.1 | 293.8 |
| 820 | | | | | | 215.1 | 275.4 | 344.2 |
| 900 | | | | | | | 302.2 | 377.8 |
| 1050 | | | | | | | 352.4 | 440.8 |
| 1100 | | | | | | | | 461.7 |
| 1200 | | | | | | | | 503.7 |
| 1310 | | | | | | | | 550.6 |
| Length to Develop Steel Yield, L _{b,rqd} [mm] | | 263 | 315 | 420 | 565 | 820 | 1,049 | 1,312 |

- 1) Design tensile steel resistance: $N_{Rd,s} = f_y * A_s / \gamma_{MS,N}$ where $\gamma_{MS,N} = 1.05$ (based on steel yield of 460 N/mm²).

 2) Design value complied in accordance to BS8110 and ACI 318 concrete splitting criteria.
- Loading data conformed to ETA-17/0410 ETAG 001 Part 1 & Part 5 Option 1. 4) Minimum spacing shall be 4d bar to bar or 5d centre-to-centre.
- 5) Minimum edge distance shall be 2d, bar to bar or 2.5d, centre-to-centre.
- 6) Applicable to dry and wet concrete application.
- 7) Design value based on non-cracked concrete.

APPROVAL LISTING





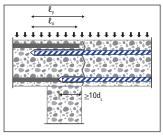


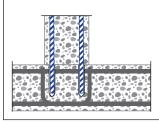


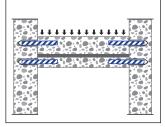


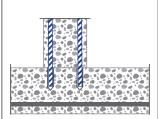


SUGGESTED APPLICATIONS









Overlap joints for slabs and beams or foundation column or wall; rebar connection for simply supported slabs or beams; shear connector or compression component joints.

